#### STANDARD RUPTURE FORMAT

Version 2.0

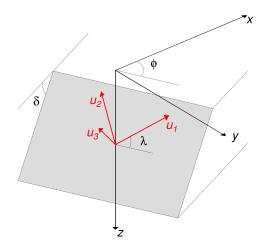
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#### Introduction

The Standard Rupture Format (SRF) is an ASCII based file format that provides a complete kinematic description for earthquake ruptures.

The general fault surface is represented by a distribution of point sources (subfaults). Each point source description contains all the necessary kinematic information to compute the contribution of that subfault to the total response of the fault rupture. In principle, there is no inherent restriction on the geometry of the fault surface or on the spacing and distribution of the point sources used to describe the fault surface. However, it is recognized that most current methods used to develop or model fault ruptures are based on descriptions that employ planar rectangular segments. To facilitate the exchange (and retention) of fault representations in this format, the description presented below allows for the (optional) inclusion of information that specifies the planar segments used to define the fault surface.

Aki & Richards convention for strike, dip and rake are used for all the source descriptions. Slip is specified in three orthogonal directions, two within the subfault surface, and the third in the direction of the outward normal to that surface. This allows for the possibility of time dependent rake and/or fault opening. Figure 1 illustrates the coordinate system conventions used in this description.



**Figure 1:** Coordinate system conventions for an individual subfault. The system (x, y, z) is the global system (e.g., x = north, y = east, z = down). The system  $(u_1, u_2, u_3)$  is the local system in which the slip is specified. The axes  $u_1$  and  $u_2$  are tangent to the rupture surface and  $u_3$  is the outward normal to the surface. The strike  $(\phi)$ , and dip  $(\delta)$  are the same as Aki & Richards. Strictly speaking, the rake  $(\lambda)$  defines the orientation of the  $u_1$  axis (with  $u_2$  at  $\lambda+90^\circ$ ).

For a pure shear dislocation with constant rake, all slip will be in the  $u_1$  direction. Incorporating time variable rake is handled using two orthogonal components ( $u_1$  and  $u_2$ ) each with a unique slip-rate function. In this case  $\lambda$  can be specified such that  $u_1$  and  $u_2$  bracket the average rake direction.

# **Version 2.0 Format Specification**

The file type as described below is in ASCII format to allow for easy exchange and editing capabilities. The general file format is as follows:

VERSION
HEADER BLOCK (optional)
DATA BLOCK

where

**VERSION** version identifier (e.g., 2.0)

**HEADER BLOCK** comments and general fault description

DATA BLOCK detailed information for all point sources covering fault surface

#### HEADER BLOCK

The optional **HEADER BLOCK** consists of a series of lines describing the general features of the rupture and fault surfaces. Comment lines are permitted in the **HEADER BLOCK** and are denoted by the '#' character appearing at the beginning of the line.

Following the comment lines, an optional description for one or more planar segments representing the fault can appear. Additional descriptive formats can be developed and added as needed.

For the planar segment format, the first line is:

PLANE NSEG

where

PLANE flag specifying that following lines describe planar fault

NSEG total number of segments in fault description

Then for each fault segment, the following two lines are needed:

ELON ELAT NSTK NDIP LEN WID

STK DIP DTOP SHYP DHYP

where (for this segment)

ELAT top center longitude

ELAT top center latitude

NSTK number of point sources (subfaults) along strike NDIP number of point sources (subfaults) down-dip

LEN segment length (km)

```
WID segment width (km)
STK segment strike
DIP segment dip
```

DTOP depth to top of fault segment (km)

SHYP along strike location (from top center) of hypocenter for this segment (km)

DHYP down-dip location (from top edge) of hypocenter for this segment (km)

The above description is repeated for each additional segment, up to the total of NSEG.

Here is an example description for a 3 segment fault:

```
PLANE 3
-119.0985
          35.0140
                   2
                        2
                            16.00
                                   12.00
  95 40
         3.00
                 -2.00
                        10.00
-118.9582 35.1398
                            30.00
                                  18.00
                 3
                        2
         0.00 -15.00
  49 80
                        10.00
-118.6702 35.2318
                           20.00
                       2
                                   15.00
                 4
 210 75 0.00 10.00 12.00
```

#### DATA BLOCK

Following the optional header lines described above are the required **DATA BLOCK** lines. The **DATA BLOCK** consists of one or more **POINT BLOCK** structures. Strictly speaking, only one **POINT BLOCK** structure is required, and it can contain the information for all of the point sources covering the fault. However, the use of multiple **POINT BLOCK** structures is convenient for describing the individual segments of a multi-segment fault rupture (i.e., one **POINT BLOCK** structure for each segment).

The first line in each **POINT BLOCK** is:

POINTS NP

where

POINTS flag specifying that following lines describe point sources (subfaults)

NP number of point sources (subfaults) to follow

Following this are blocks of lines containing information about each of the NP point sources (subfaults). The format of the lines in each of these NP blocks is:

LON	LAT	DEP	STK	DIP	AREA	TINIT	DT	VS	DEN
RAKE	SLIP1	NT1	SLIP2	NT2	SLIP3	NT3			
SR1[1]	SR1[2]	SR1[3]		SR1[NT1]					
SR2[1]	SR2[2]	SR2[3]		SR2[NT3]					
SR3[1]	SR3[2]	SR3[3]		SR3[NT3]					

where

LON longitude of subfault center
LAT latitude of subfault center
DEP depth of subfault center (km)

STK strike DIP dip

AREA area of subfault (cm<sup>2</sup>)

TINIT initiation time when rupture reaches subfault center (sec)

DT time step in slip velocity function (sec)

VS shear wave velocity at source point (cm/sec), enter -1 if not known

DEN density at source point (g/cm<sup>3</sup>), enter -1 if not known

RAKE direction of u<sub>1</sub> axis (rake direction)

SLIP1 total slip in u<sub>1</sub> direction (cm)

NT1 number of time points in slip rate function for u<sub>1</sub> direction

SLIP2 total slip in u<sub>2</sub> direction (cm)

NT2 number of time points in slip rate function for u<sub>2</sub> direction

SLIP3 total slip in u<sub>3</sub> (surface normal) direction (cm)

NT3 number of time points in slip rate function for  $u_3$  direction SR1[1],...,SR1[NT1] slip rate at each time step for  $u_1$  direction (cm/sec) SR2[1],...,SR2[NT2] slip rate at each time step for  $u_2$  direction (cm/sec) SR3[1],...,SR3[NT3]

Although the general format given here allows for slip in all three directions  $(u_1, u_2, u_3)$ , most cases will have only one  $(u_1)$  or two  $(u_1, u_2)$  non-zero slip components. In these situations, the remaining slip components, as well as the number of time points for the slip rate function, are specified as "0".

### **Changes from Version 1.0**

- 1. Added option to specify comment lines within the **HEADER BLOCK**. Comment lines are denoted with a leading '#'.
- 2. Added fields for VS (shear wave velocity in cm/sec) and DEN (density in g/cm³) to the subfault description. Values for these parameters may not always be available (e.g., for scenario ruptures generated for an unspecified region), in which case a value of -1 should be entered.
- 3. Added option to subdivide the specification of the individual point source descriptions into multiple POINT BLOCK structures (version 1.0 requires that the subfault descriptions for all fault segments be included in a single POINT BLOCK structure).

# **Examples**

# Example 1: Single Point Source

```
2.0
# Example 1: This is an example of the simplest form of a SRF file.
# This file represents a point source with strike=291, dip=59 and rake=142.
# Since the source is represented kinematically, it has a slip (16.32 cm)
\# over an area (2.64926e+11 cm*cm) with rigidity given by Vs*Vs*den
\# [(3.64e+05 \text{ cm/s})*(3.64e+05 \text{ cm/s})*(2.67 \text{ g/cm}^3)=3.54e+11 \text{ dyne/cm}^2].
# This gives a seismic moment of 1.53e+24 dyne-cm (Mw 5.42).
\# The slip-rate function is a simple isosceles triangle discretized at 0.025 sec.
# Note that the slip-rate function is zero for all time points after those
\# listed in the file (i.e., the last time point is implicitly zero and
# is not included).
# Other useful information that might be included in these comment lines is documentation
# of the source of the rupture e.g.,
       "Example 1 is a sample SRF generated by hand on Fri Nov 21 12:52:16 PST 2014
       (Robert Graves, <rwgraves@usgs.gov>)."
# or the usable bandwidth of the rupture, e.g.,
      "This model is applicable in the bandwidth T>10 sec."
POINTS 1
-117.7610 33.9530 14.70 291 59 2.64926e+11 0.0000 2.50000e-02 3.64000e+05 2.67000e+00
```

### Example 2: Single Planar Fault

```
2.0
# Example 2a: Single planar fault.
# Following these comment lines, a description of the fault plane location and
# geometry is given by 3 lines starting with "PLANE 1". Note that this description
# of the fault plane is optional. However, this information is useful in that it
# provides a concise description of the fault (e.g. for plotting purposes, etc.).
# The kinematic rupture information begins with the line "POINTS 4", which means this
# rupture is represented by 4 subfaults. The detailed description of the rupture on
# each subfault follows this line. Note that each subfault has a single slip-rate
# function with the direction of slip (rake) varying from subfault to subfault.
# Other useful information that might be included in these comment lines is documentation
# of the source of the rupture e.g.,
       "Example 2a is a sample rupture scenario generated Mon Nov 24 11:50:22 PST 2014
       with the code "genslip-v3.3.2" (Robert Graves, <rwgraves@usgs.gov>)."
# or the usable bandwidth of the rupture, e.g.,
       "This rupture is applicable in the bandwidth T>3 sec."
PLANE 1
-119.0985 35.0140 2
                             2 16.00
                                           12.00
            3.00 -2.00 10.00
 95 40
POINTS 4
-119.1459 34.9826 4.9284 95 40 4.80000e+11 2.6465 1.00000e-01 3.20000e+05 2.65000e+00 82 8.59 6 0.00 0 0.00 0 0.00000e+00 5.91682e+01 1.16849e+01 8.57081e+00 4.81257e+00 1.63265e+00
 -119.0585 34.9763 4.9284 95 40 4.80000e+11 2.4801 1.00000e-01 3.20000e+05 2.65000e+00
120 43.18 7 0.00 0 0.00
                                                  Ω
  0.00000e+00 2.88510e+02 5.43680e+01 4.31742e+01 2.83736e+01 1.38752e+01
  3.50832e+00
 -119.1503 34.9414 8.7851 95 40 4.80000e+11 0.0000 1.00000e-01 3.60000e+05 2.75000e+00
 76 26.61 2 0.
0.00000e+00 2.66114e+02
                2 0.00
                                 0.00
                                                  0
 -119.0629 34.9352 8.7851 95 40 4.80000e+11 0.1637 1.00000e-01 3.60000e+05 2.75000e+00
  82 118.54 9 0.00 0 0.00
                                                  0
  0.00000e+00 6.18123e+02 2.28298e+02 1.12802e+02 9.21321e+01 6.71185e+01 4.17206e+01 1.99587e+01 5.27757e+00
```

### Example 3: Multi-segment Rupture

```
2.0
# Example 3a: Multi-segment fault rupture (3 segments).
# This rupture consists of 3 planar rectangular segments. Following these comment lines,
# a description of the location and geometry of the individual fault segments is given by
# 7 lines starting with "PLANE 3"; 2 lines for each of the 3 fault segments. Note that
# this description of the fault segments is optional. However, this information is useful in
# that it provides a concise description of the fault (e.g. for plotting purposes, etc.).
# The kinematic rupture information for each segment begins with a line "POINTS <NP>".
# There are 3 of these in this file, one for each segment, and the detailed subfault
# information for each segment follows the "POINTS <NP>" line. The number of subfaults
# (<NP>) can be different for each segment (<NP>= 4, 6, 8, respectively for the
# 3 segments in this file).
# Other useful information that might be included in these comment lines is documentation
# of the source of the rupture e.g.,
                 "Example 3a is a sample rupture scenario generated Mon Nov 24 12:19:29 PST 2014
                   with the code "genslip-v3.3.2" (Robert Graves, <rwgraves@usgs.gov>)."
# or the usable bandwidth of the rupture, e.g.,
                 "This rupture is applicable in the bandwidth T>8 sec."
PLANE 3
                            35.0140
  -119.0985
                                                           2.
                                                                           2
                                                                                         16.00
                                                                                                              12.00
                                                                            10.00
                                 3.00 -2.00
    95 40
                             35.1398 3
                                                                                                               18.00
                                                                        10.00
                                0.00 -15.00
   49 80
                                                                       2 20.00
12.00
                             35.2318 4
  -118.6702
 210 75
                                0.00 10.00
POINTS 4
  -119.1459 34.9826 4.9284 95 40 4.8000e+11 3.9808 5.00000e-01 -1.00000e+00 -1.00000e+00
    90 78.56 3 0.00 0 0.00
                                                                                                                               Ω
   0.00000e+00 1.15372e+02 4.17567e+01
  -119.0585 34.9763 4.9284 95 40 4.8000e+11 3.9946 5.00000e-01 -1.00000e+00 -1.00000e+00
     94 124.76
                                         3 0.00 0
                                                                                                    0.00
    0.00000e+00 1.86001e+02 6.35258e+01
  -119.1503 \quad 34.9414 \quad 8.7851 \quad 95 \quad 40 \quad 4.8000 \\ e+11 \quad 0.0000 \quad 5.00000 \\ e-01 \quad -1.00000 \\ e+00 \quad -1.000000 \\ e+00 
    20 248.43 2 0.00 0
                                                                                                    0.00
    0.00000e+00 4.96865e+02
  -119.0629 34.9352 8.7851 95 40 4.8000e+11 4.6669 5.00000e-01 -1.00000e+00 -1.00000e+00
                                                            0.00
                  0.00
                                                                                   Ω
 115
                                                                                                    0.00
POINTS 6
  -118.9772 \quad 35.0207 \quad 4.4316 \quad 49 \quad 80 \quad 9.0000e + 11 \quad 8.5605 \quad 5.00000e - 01 \quad -1.00000e + 00 \quad -1.000000e + 00 \quad -1.00000e + 00 \quad -1.000000e + 00 \quad -1.00000e + 00 \quad -1.00000e + 00 \quad -1.000
              81.21 3 0.00 0
                                                                                                     0.00
                                                                                                                              0
  0.00000e+00 1.06553e+02 5.58618e+01 
-118.8944 35.0797 4.4316 49 80 9.0000e+11 11.7304 5.00000e-01 -1.00000e+00 -1.00000e+00
  -11 102.76
                                                         0.00
                                                                                   0
                                                                                                   0.00
   0.00000e+00 1.44288e+02 6.12220e+01
  -118.8115 35.1386 4.4316 49 80 9.0000e+11 16.1476 5.00000e-01 -1.00000e+00 -1.00000e+00
                                         2 0.00
      7 61.28
                                                                                    Ο
                                                                                                     0.00
   0.00000e+00 1.22558e+02
  -118.9659 35.0102 13.2949 49 80 9.0000e+11 6.0000 5.00000e-01 -1.00000e+00 -1.00000e+00
  -48 302.30
                                                            0.00
                                                                                 0.00
   0.00000e+00 3.70640e+02 2.02352e+02 3.16073e+01
  -118.8831 35.0691 13.2949 49 80 9.0000e+11 12.2177 5.00000e-01 -1.00000e+00 -1.00000e+00
                  0.00 0 0.00
                                                                                 0 0.00
  -118.8002 35.1280 13.2949 49 80 9.0000e+11 14.2068 5.00000e-01 -1.00000e+00 -1.00000e+00
     60 130.10
                                        2 0.00
                                                                                  0
                                                                                                  0.00
    0.00000e+00 2.60198e+02
POINTS 8
 -118.6980 35.3227 3.6222 210 75 3.7500e+11 24.2740 5.00000e-01 -1.00000e+00 -1.00000e+00 52 62.62 3 0.00 0 0.00 0
    0.00000e+00 8.55161e+01 3.97197e+01
```

-118.7255 35.2838 3.6222 210 75 3.7500e+11 20.3903 5.00000e-01 -1.00000e+00 -1.00000e+00 73 259.66 6 0.00 0 0.00 0 0.00000e+00 3.57517e+02 7.02898e+01 5.18295e+01 2.94211e+01 1.02659e+01 -118.7530 35.2449 3.6222 210 75 3.7500e+11 20.5304 5.00000e-01 -1.00000e+00 -1.00000e+00 58 89.32 3 0.00 0 0.00 0 58 89.32 3 0.00 0 0 0.00000e+00 1.20825e+02 5.78088e+01 -118.7805 35.2060 3.6222 210 75 3.7500e+11 18.2282 5.00000e-01 -1.00000e+00 -1.00000e+00 22 173.57 4 0.00 0 0.00 0 0.00000e+00 2.04059e+02 1.03183e+02 3.98911e+01 -118.7165 35.3314 10.8667 210 75 3.7500e+11 21.5693 5.00000e-01 -1.00000e+00 -1.00000e+00 90 138.38 2 0.00 0.00 0.00000e+00 2.76766e+02  $-118.7440 \quad 35.2925 \quad 10.8667 \quad 210 \quad 75 \quad 3.7500 \\ e+11 \quad 20.7451 \quad 5.00000 \\ e-01 \quad -1.00000 \\ e+00 \quad -1.00000 \\ e+0$ 45 77.84 2 0.00 0 0.00 0 0.00000e+00 1.55686e+02 -118.7715 35.2536 10.8667 210 75 3.7500e+11 18.3628 5.00000e-01 -1.00000e+00 -1.00000e+00 -15 102.13 3 0.00 0 0.00 0 0.00000e+00 1.33963e+02 7.02981e+01 -118.7990 35.2147 10.8667 210 75 3.7500e+11 18.0000 5.00000e-01 -1.00000e+00 -1.00000e+00 35 0.00 0 0.00 0 0.00 0